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ZOOM LENS**BACKGROUND OF THE INVENTION**

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1. Field of the Invention

The invention relates to a zoom lens comprising in a direction of light propagation a front lens group having positive refractive power, a variator lens group having negative refractive power, a compensator lens group having positive refractive power, a base lens group having positive refractive power.

15 Numerous zoom lenses are already known from the prior art. The zoom lenses must fulfil specific optical and/or mechanical properties, depending on requirement.

2. Description of the Related Art

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Zoom objectives for photography typically have a zoom factor of 2 to 4. The exit pupil vision is not telecentrically configured here. The installed length is to be kept as short as possible with these zoom lenses.

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Furthermore, zoom lenses for video recordings, for example camcorders, are known from the general prior art. The CCD detectors used in this case have an image diameter of at most 11 mm. The zoom factor is specified 30 here mostly as 10, the focal range reaching from 3 mm to 50 mm in known makes.

The zoom factor for such lenses is approximately 20 to 30 in the case of zoom lenses for television recordings. The CCD detectors used in this case have an image diameter of typically 11 mm. Focusing is performed here by the front group, as a rule. These lenses must have a long back focus in order to be able to in-

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stall a color-splitting prism between a last lens and a detector.

Afocal zoom lenses are frequently used as component
5 parts in instrumental optics. The diaphragm position can be varied during the zooming operation in the case of such systems.

None of the zoom lenses enumerated corresponds per se
10 to the desired characteristics of a zoom lens for military reconnaissance. It is also impossible to create other characteristics for the said zoom lenses by a few and simple conversions by means of known optical computing programs. Moreover, the multiplicity of afocal
15 zoom lenses have a smaller diameter to achieve a constant aperture number over a focal range of up to approximately 280 mm in combination with a lens of suitable focal length.

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SUMMARY OF THE INVENTION

Consequently, it is an object of the invention to create a zoom lens that fulfills the requirements with reference to optical properties and focusing characteristics,
25 the aim being for the installation space, of which only a limited amount is available, to be kept as small as possible, and for the zoom lens to be capable of functioning in a temperature range from -35°C to +75°C.

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According to the invention, this object is achieved by virtue of the fact that the base lens group comprising a first base lens group and a second base lens group, wherein the front lens group, the variator lens group,
35 the compensator lens group and the first base lens group are arranged along a common straight first optical axis, wherein the second base lens group is arranged along a second optical axis inclined with re-

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spect to the first optical axis at a first angle α different from 0° and 180° , and wherein a beam deflector is arranged between the first base lens group and the second base lens group.

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The zoom lens comprises a front lens group, a variator lens group, a compensator lens group and a base lens group, the base lens group being split into two groups with a positive refractive power in each case. Splitting the base lens into two produces a relatively large air space between the first base lens group and the second base lens group. The second base lens group of the base lens group is arranged at a specific angle α to the first base lens group of the base lens group, it being advantageously possible thereby for an at least approximately L-shaped arrangement of the zoom lens to be produced. A plane mirror for beam deflection is advantageously located in the air space between the first base lens group and the second base lens group.

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Such an arrangement can be used to implement the special characteristics for a zoom lens for military reconnaissance, the result being a zoom lens of high imaging quality, compact installation space because of the angle α , large zoom factor and large spectral range.

It can be provided advantageously that the first base lens group and the second base lens group are arranged at a distance along the first and second optical axis, which distance is at least 15% of the overall length of the zoom lens, measured from a vertex of the front lens group to the back focal plane of the base lens group.

35 The refractive powers of the two groups of the base lens group are to be selected such that as large an air space as possible is permitted between the two groups.

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The air space should be at least 15% of the installed length of the zoom lens. It is thereby possible that a beam deflector can be introduced into this air space, and thus that an installation space as small and compact as possible is created.

With a design principle according to the invention it is possible to design zoom lenses for military reconnaissance which should have specific optical properties such as, for example, a zoom factor of 8, a variable focal range of 34 mm to 272 mm, an aperture number of at least 3.2 and, in a wavelength region from 450 nm to 750 nm, an outstanding optical imaging quality. Moreover, special mechanical properties, such as integration in a compact installation space, must be created for such zoom lenses. An important role is played, furthermore, by the environmental conditions. Zoom lenses for military reconnaissance must ensure they can function in a wide temperature range from intense cold to excessive heat.

Advantageous embodiments and developments emerge from the further subclaims and the exemplary embodiment described below in principle with the aid of the drawing, in which:

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 shows an illustration of the principle of a zoom lens for military reconnaissance (lens section); and

Figures 2a show a lens section of a zoom lens of three focal length settings, where figure 2a corresponds to $f = 34$ mm; figure 2b corresponds to $f = 122$ mm and figure 2c corresponds to $f = 272$ mm.

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DETAILED DESCRIPTION

- Figure 1 shows an illustration of the principle of an inventive zoom lens ZO in lens section for military reconnaissance. The zoom lens ZO comprises a front lens group G1 of positive refractive power, a variator lens group G2 of negative refractive power, a compensator lens group G3 of positive refractive power, a base lens group G4 of positive refractive power and an optical spectral filter 20. The front lens group G1 is constructed from a negative lens 1 and two positive lenses 2 and 3. The negative lens 1 and the positive lens 2 are a split cemented component. This is advantageous because of the large difference in the coefficient of thermal linear expansion α of the two lenses 1 and 2. The positive lenses 2 and 3 are made from FluorCrown (FK) or a comparable material with respect to abnormal partial dispersion.
- The variator lens group G2 comprises two cemented components, each cemented component having a negative refractive power. The positive lenses 4 and 7 of the two cemented components are made from high-index dense flint (SF) glasses of long-crown type. A type of glass is long crown when it holds that $\Delta P_{g,F} > 0$ for the deviation of the relative partial dispersion $\Delta P_{g,F}$ from the normal straight line. The negative lenses 5 and 6 are of short flint type such as, for example, the dense lanthanum flint (LaSF). Thus, a glass is of short flint type when it holds that $\Delta P_{g,F} < 0$ for $\Delta P_{g,F}$.

The compensator lens group G3 is preferably designed as a cemented component of a positive lens 8 and a negative lens 9.

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The base lens group G4 is divided into two groups, wherein a first base lens group G4.1 is arranged along

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- a first optical axis 23 and a second base lens group G4.2 is arranged along a second optical axis 23'. The second optical axis 23' is inclined with respect to the first optical axis 23 at a first angle α different from 5 0° and 180° . In the zoom lens according to the example $\alpha = 75^\circ$. A relatively large air space for introducing a beam deflector 18 for beam deflection is provided between the first base lens group G4.1 and the second base lens group G4.2. The beam deflector 18 is a plane 10 mirror with a mirror surface having a normal to the mirror surface 18' wherein the normal to the mirror surface 18' being inclined to the first optical axis 23 at a second angle which is a half of the first angle α .
- 15 The distance between the first base lens group G4.1 and the second base lens group G4.2 should amount to at least 15% of the overall length of the zoom lens ZO measured from a vertex of the front lens group G1 to a back focal plane of the base lens group G4. The beam is 20 deflected by 105° in this exemplary embodiment. The result is a L-shaped structure of the zoom lens ZO. The two limbs of the L-shaped installation space thereby form an acute angle α of 75° . The beam deflection can, of course, also be performed by a deflecting prism instead of the plane mirror 18.

An iris diaphragm 19 is arranged in the direction of light propagation between the compensator lens group G3 and the first base lens group G4.1. The iris diaphragm 30 19 is imaged by the base lens group G4 such that its image appears virtually at infinity (∞). Because of pupil aberrations, it is not possible to produce on the image side a telecentric beam profile for all centroid rays 22 which are illustrated in figures 2a to 2c. The 35 ray that runs centrally between an upper and a lower coma ray is designated as centroid ray 22. The iris

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diaphragm 19 should be positioned such that a deviation from telecentricity is as small as possible. The deviation from telecentricity should be at most 1.7° .

- 5 The position and size of the iris diaphragm 19 are not changed during the variation in focal length. This means the distance of the diaphragm to the first base lens group G4.1 is fixed during zooming.
- 10 Lens sections are illustrated in figures 2a to 2c for three focal length settings.
In figure 2a, the focal width is $f = 34$ mm. The first base lens group G4.1 of the base lens group G4 has a positive refractive power and comprises a single lens 10 of positive refractive power and a cemented component that is assembled from the lens 11 and 12 and is of positive refractive power. The single lens 10 is produced from FluorCrown (N-FK51). The positive lens 12 in the cemented component is made from dense phosphate crown (N-PSK53), and the negative lens is made from lanthanum flint (N-LAF2). The relationships between the types of glass are in accordance with the Schott glass catalogue. The lenses 10, 11 and 12 can, of course, also be produced from other types of glass with comparable characteristics. It is important to heed in this case the abnormal partial dispersion. If glasses from other manufacturers, for example OHARA, are used, it must be borne in mind that the refractive index n_d , dispersion v_d and the abnormal partial dispersion $\Delta P_{g,F}$ deviate by at most 10%.

The second base lens group G4.2 of the base lens group G4 is of positive refractive power overall and preferably serves as a focusing group. The second base lens group G4.2 can be moved along the second optical axis 23' for focussing in order thus to hold the image position, which is displaced in the event of a change in

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- temperature and air pressure. Since the refractive indexes, the thicknesses and the radii of the individual lenses are a function of temperature, the image position is displaced in the event of a change in temperature and air pressure. At high temperatures, for example approximately +60°C, the image position is no longer situated in a detector plane 21, but behind the latter. At low temperatures of approximately ~20°C, the image plane is likewise not located in the detector plane 21, but between the optical spectral filter 20 and the detector plane 21. Likewise, objects situated close by can be sharply focused using the focusing group G4.2. Consequently, an internal focusing is implemented with the aid of which it is possible to balance out the changes in temperature and air pressure, and it is likewise possible to focus on objects situated close by. The variation in focal length and the internal focusing are independent of one another.
- The focusing group G4.2 comprises a meniscus-shaped lens 13, a positive lens 14 that is produced from FluorCrown (FK), a cemented element composed of the two lenses 15 and 16, and a negative lens 17. The glass of the meniscus-shaped lens 13 is of long-crown type. The glass of the negative lens 17 is of short flint type.

The optical spectral filter 20 is an absorption filter consisting of a colored glass with a vapour-deposited edge filter. The optical spectral filter 20 is arranged between the second base lens group G4.2 and the back focal plane of the base lens group G4. The colored glass is preferably a yellow glass. This longpass filter glass is distinguished in that it has low transmission in the short wave spectral region and high transmission in the long wave spectral region. Of course, it is possible here to select with reference to the colored glass used which spectral region is to be passed and which is to be blocked. The yellow glass corre-

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spondingly attenuates the blue and violet light. Consequently, the colored glass restricts the spectral region beyond ultraviolet (UV). Other colored glasses can also be used in principle. Slight differences in the refractive index of the colored glasses can be compensated with the aid of the second base lens group G4.2 without loss of imaging quality. The vapour-deposited edge filter limits the spectral region beyond infrared (IR). The zoom lens according to the invention is designed here for the spectral region from 450 nm to 750 nm. A smaller spectral region can be selected within this region by selection of colored glass and edge displacement. It is also possible to displace the spectral region to 500 nm to 850 nm. The change in the image position can be compensated by using the second base lens group G4.2.

For specific applications, for example for a periscope in submarines, it is necessary to produce an image offset on the detector 21. The image offset is achieved by tilting or rotating the optical spectral filter 20 around the second optical axis 23'. There should be a large filter thickness in order to keep the tilting angle as small as possible.

The air space between the last lens 17 of the base lens group G4 and the detector 21 should be optimized with regard to focusing movement of the second base lens group G4.2, the thickness and the rotary or tilting movement of the optical spectral filter 20 and of the installation space of the detector 21, depending on the special characteristic and focal length of the zoom lens ZO.

The refractive power and the position of the front main plane of the split base lens group G4 image the iris diaphragm 19, located at a short distance in front of the base lens group G4, to infinity or virtually to in-

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finity. The position of the iris diaphragm 19 should not be changed during the zooming operation, since the iris diaphragm 19 limits the rays impinging on the basic lens group G4. The iris diaphragm 19 should be introduced in the zoom lens ZO such that the precondition of telecentricity is retained on the detector 21.

At a specific site, use is made in the individual lens groups of the zoom lens ZO of glasses of long-crown or short flint type. It should be borne in mind with types of glasses that are to be cemented together that the difference in the coefficient α of the thermal linear expansion of the two types of glass is smaller than $2.5 \cdot 10^{-6}/K$, since the zoom lens ZO is used in a relatively wide temperature range. If the difference in the thermal coefficients of linear expansion of the two types of glass is greater than $2.5 \cdot 10^{-6}/K$, it is impossible for the types of glass to be permanently cemented.

For short focal lengths of the zoom lens ZO, attention centres on the correction of the transverse chromatic aberration, since the image-side principle ray is inclined to the optical axes 23 and 23' as a function of color in the image of an object point remote from the axis. The transverse chromatic aberration leads to a linear magnification for each color. In the case of long focal lengths of the zoom lens ZO, attention should be centred on the correction of the longitudinal chromatic aberration, since the focal length of the zoom lens ZO is a function of the frequency of the light. Consequently, the focal length for short wave, that is to say blue light is lower than that for long wave, red light. However, a color correction can be fully achieved when types of glass with abnormal partial dispersion are used. Such glasses are either of long-crown type or short flint type.

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- The front lens group G1, the variator lens group G2, the compensator lens group G3 and the first base lens group G4.1 of the base lens group G4 are arranged in
5 the long limb of the L-shaped installation space along the common straight first optical axis 23. The second base lens group G4.2 of the base lens group G4, the optical spectral filter 20 and the detector 21 are integrated in the short limb of the L-shaped installation
10 space. The long limb has a maximum length of 245 mm, the short limb having a maximum length of 115 mm. The lengths of the limbs can be varied depending on the design desired for the zoom lens ZO.
- 15 The available installation space for the lenses of the groups G1, G2, G3 and G4 are further limited by the position and size of the plane mirror 18 or the deflecting prism, and by the constrictions applying in the air space between the lens 17 and the detector 21. The diameter of the front lens group G1 should be at most
20 90 mm, that of the variator lens group G2, of the compensator lens group G3 and of the base lens group G4 should be limited to at most 45 mm.
- 25 In figure 2b, the focal length of the zoom lens ZO is $f = 122$ mm. In order to be able to realize this focal length, the variator lens group G2 and the compensator lens group G3 are displaced in the direction of the first base lens group G4.1 of the base lens group G4 along the first optical axis 23. The distance between
30 the variator lens group G2 and the compensator lens group G3 has become minimally smaller by comparison with figure 2a.
- 35 The focal length of the zoom lens ZO is $f = 272$ mm in figure 2c. The aperture number is 3.2 here. In order to achieve a focal length of $f = 272$ mm, the variator lens group G2 is displaced right up to the compensator lens

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group G3 along the first optical axis 23. As in figures 2a and 2b, here, as well, a cone 22' and a centroid ray 22 of a further cone (not illustrated) are imaged in order to display the optical path.

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The first angle α between the long limb and the short limb of the L-shaped installation space is 75° in all three figures. The first angle α can also be of variable design, wherein the first angle α should be preferably in the range between 50° and 130° . For example, the first angle α can have a value of 85° , although it should be borne in mind that the focusing characteristics can still be realized. If there is no precondition limiting the installation space, it is also possible that there need be no beam deflection. Consequently, there is also no need for a plane mirror 18 for beam deflection.

A CCD detector whose image diagonals are 21.45 mm is used as receiver 21.

It is possible with the aid of this design to implement a zoom lens ZO that satisfies the requirements with reference to the zoom factor, the focal range, the aperture number, the image diameter, the telecentric position of the exit pupil and the focusing characteristics, for example, for military reconnaissance. Moreover, a very good polychromatic correction of the zoom lens ZO can be achieved with the aid of this design.

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